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.24 MAY 1948

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE

No. 1438

EFFECT OF SIMULATED SERVICE CONDITIONS ON PLASTICS
DURING ACCELERATED AND 2-YEAR

WEATHERING TESTS

By W. A. Crouse, D. C. Caudill, and F. W. Reinhart

National Bureau of Standards

FOR REFERENCE

NOT TO BE TAKEN FROM THIS ROOM

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SUMMARY

The effects of outdoor weathering for 2 years and of an accelerated weathering test on the weight, dimensional stability, and flexural properties of selected reinforced plastics were investigated. The results of all tests, both in this report and the previous report (NACA TN No. 1240), indicate that none of the laboratory aging tests correlated with outdoor weathering with respect to all properties and all materials.

INTRODUCTION

This report supplements information given in a previous report on this same subject (reference 1). The results of a 2-year outdoor weathering test and an accelerated weathering test (Method 6023, reference 2) on the weight, dimensional stability, and flexural properties of selected reinforced plastics are presented.

This investigation, conducted at the National Bureau of Standards, was sponsored by and conducted with the financial assistance of the National Advisory Committee for Aeronautics.

MATERIALS AND TEST PROCEDURES

The materials tested were the same as those used in the tests previously reported in reference 1. A description of the materials is given in table I, which has been reproduced from reference 1 for convenience. The dimensions of the specimens were also the same as those described in reference 1.

The 2-year outdoor weathering test was a continuation of the 1-year test previously reported (reference 1).

The accelerated weathering test was made in accordance with Method No. 6023 of Federal Specification L-P-406a (reference 2). This test involves exposure to cycles of soaking, freezing, drying, and radiation rich in ultraviolet-light. The conditions used in this test are as follows:

- (a) $2^{\frac{1}{4}}$ hours at 100° F (38° C) over water (b) $^{\frac{1}{4}}$ hours at $^{-70^{\circ}}$ F (-57° C) (c) $^{\frac{1}{6}}$ hours at $^{\frac{1}{60^{\circ}}}$ F (71° C)
- (d) 4 hours of exposure to ultraviolet radiation

In (a) the condition was obtained by suspending the specimens individually over water in 8-ounce bottles. In (b) and (c) the low and high temperatures were attained by placing the specimens in a lowtemperature test cabinet and in a circulating-air oven, respectively. In (d) the source of ultraviolet radiation was an S-1 bulb in a sunlamp, as specified in Method No. 6021 of reference 2. During this part of the cycle the specimens were turned end for end every 2 hours to obtain more uniform exposure to the radiation over the entire length. The bolts and nuts above the disk were arranged so as to-be suitable for holding the 1- by 3-inch specimens.

The weight and dimensions of one set of specimens were measured within 10 minutes after the conclusion of 1, 3, 5, and 10 cycles. The flexural properties were determined on other sets at the end of 5 and 10 cycles, respectively, after conditioning at 77° F and 50-percent relative humidity for 48 hours.

RESULTS AND DISCUSSION

Weight and Dimensional Changes

The percentage changes in weight, length and width, and thickness of the materials on exposure to the 2-year outdoor weathering and accelerated weathering tests are shown in table II. In most instances the percentage changes in weight, length, width, and thickness decreased. Of those showing increases, most were observed in thickness.

Comparing the accelerated service tests generally, test IV caused the greatest changes followed by accelerated weathering test 6023; it is to be noted, however, that the effects of accelerated tests are different from the outdoor weathering test as shown by the differences in the rankings (table III) for the outdoor and for the accelerated service tests.

The relative weight and dimensional stability of the various materials are shown in table III. The results of aging tests shown in table V of reference l are incorporated into this table for comparison. The rating method is the same as used in reference 1.

Changes in Flexural Properties

The percentage changes in flexural strength, flexural modulus of elasticity, and maximum deflection in flexure of the materials on exposure to the 2-year outdoor weathering and accelerated weathering tests are shown in table IV.

Considering the tests shown in table TV of reference 1 and table TV of the present report, the 10-cycle accelerated service test TV gives percentage changes in flexural strength of approximately the same order of magnitude as the 2-year outdoor weathering and is the most severe of the aging procedures with respect to changes in flexural strength. However, the rankings of different materials for the outdoor weathering and accelerated weathering test TV are not in concordance.

The relative retention of flexural strength by the various materials is shown in table III. The aging tests shown in table V of reference l are incorporated into this table for comparison. The rating method is the same as used in reference 1.

Correlation of Laboratory Aging Tests

with Outdoor Weathering

Correlation coefficients of rank were obtained by comparing the rankings of the plastics for the accelerated weathering tests with the rankings for the outdoor weathering tests. No accelerated weathering tests correlated with the outdoor weathering tests sufficiently well to be regarded in any way as a useful substitute. It is worth noting that the five accelerated service tests show concordance among themselves to a statistically significant extent, though they do not reproduce the ranking of the outdoor weathering tests.

CONCLUSION

A comparison of the degree of correlation of the results obtained in the various laboratory aging procedures with those observed in the 1- and 2-year exposure tests out of doors, confirms the previous conclusion that none of the laboratory tests give results with all the materials and for all the properties which correlate with the results of outdoor weathering.

National Bureau of Standards
Washington, D. C., April 16, 1947

REFERENCES

- 1. Crouse, W. A., Caudill, D. C., and Reinhart F. W.: Effect of Simulated Service Conditions on Plastics. NACA TN No. 1240, 1947.
- 2. Federal Specification L-P-406a: Plastics Organic; General Specifications, Test Methods; Jan. 24, 1944. Government Printing Office, Washington 25, D. C.

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TABLE I.- DESCRIPTION OF MATERIALS

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From reference il

											•	
	Good 4ng	(ntm)	ĸ.						Gradual	&	82	·&
Time	Cimelno	Guring (min)							2 hours at 158° F 10 hours at 158-239° F	8	ξ.	8
lone	Curing temperature Initial Maximum (OF)		380						କ୍ଷ	· 9£	8	946
Molding conditions	Curing ter Initial (°F)		SC Sc						158		-	
Molds	Pressure (lb/sq in.)		8100	250	0 <u>0</u>				2-1 2-1	1800	1620	1800
	<u>ر</u> 10	plies	,				!	۲-	•	t	13	r .
	Ply arrengement		 	Parallel	Crossed		Crossed		Стовней	Crossed	Parallel	Parallel
Reinforcement	Thread count	Warp Filling	ı	i	;	Į.	7.1	8 1 1	35	Q.	8	91
olufor	in in	Warr	ŀ	1	·	i	8	2	36	8	8	18
1	Туре		Macerated cotton fabrio	Рарог	Рарвг	Lignin paper	Glass febrio, plain weave E00-11-162	<pre>Cotton fabric (malin), twill weave</pre>	Ootton fabrio (emmoled duok), plain weave	Cotton fabric, plain weave, 10 or/eq yd	Cotton fabric, plain weave, 3.7 oz/sq yd	Asbestos fabrio, plain weave, 18 oz/se yd
ū	Content by weight (percent)								62-63	84	94 97	14
Regin	Type		Bakelite RM-1,99			Lignin	Marco MR-1A	Marco MR-1A	Allymor CR39	Bakelite No. 1112	Balcalite BV-1112	Bakelite No. 2427
	Density	(e/ or or	1.37	1.43	1.43	1,38	1.70	1.27	1.37	1.36	46°-1	1.30
	Average thickness	(in.)	121.0	क्षाः	†टा:	326.	911.	ır.	541.	ă	धुं	64T
	Manufaoturer		Bakelite Corp.	Consolidated Water Power and Paper Co.	Consolidated Water Power and Paper Co.	Formica Insulation Go.	Swedlow Aeroplastics Corp.	Swedlow Aeroplastics Corp.	Pittsburgh Plate Glass Co., Columbia Chemical Division	Synthane Corp.	Synthens Corp.	Bynthene Carp.
	Type of leminate.		Macerated-cotton-fahric Bakelite Corp. phenolic molding compound	High-strength paper,	High-strength paper, phenolic	Lignin paper	Glass-fabric, unsabrated polyester	Muslin-cotton-fabric, unsaburated polyester	Enemeled-duck cotton- fabric, unsaturated polyester	Grade C phenolic	Grade I phenolin	Grade AA phenalic
	MBS naterial designation		ą.	a	ថ	검	#	E .	Ħ.	#	r,	¤

Asterial Al was obtained in the form of sheets prepared from a molding compount; all of the other materials were lastrated sheet products.

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TABLE II. - CHANGES IN WEIGHT AND DIMENSIONS OF PLASTICS DURING OUTDOOR AND ACCELERATED WEATHERING TESTS

Material desig-	Change during outdoor weathering test,	Changes during accelerated weathering test (b)								
nation	2 years (percent) (a)	l 3 cycle cycles (percent) (percent)		5 cycles (percent)	10 cycles (percent)					
Al Blc Bld Cl Dl El Fl HL Jl	-1.05 1.63 1.68 1.52 .30 49 22 20 79 92	-2.26 73 79 85 -1.34 -1.50 -1.27 -1.70 -1.42 -1.22	-3.10 62 76 87 -1.70 43 -1.58 -2.25 -1.88 -1.36	-3.44 65 81 97 -1.88 47 -2.00 -1.69 -2.47 -2.12 -1.38	-3.98 76 98 -1.13 -2.10 56 -2.26 -1.93 -2.74 -2.42 -1.36					
Length and width										
Al Bl ^C Bl ^d Cl Dl El Hl Il Jl	-0.18 16 20 16 12 02 22 18 12 11	-0.26 14 14 08 16 .00 20 19 16 14 07	-0.38 16 14 10 20 .00 24 26 22 20	-0.44 16 14 10 23 .00 28 29 26 22	-0.54 18 20 08 30 .00 36 36 15 30 13					
		Thicknes	38 							
Al Blo Bld Cl Dl El Fl Hl Jl Kl	0.46 4.33 4.85 4.06 1.10 .39 1.17 .96 05 03	-0.04 .22 .27 .03 18 .28 19 .11 13 08 05	-0.04 .55 .43 .14 11 .10 08 .02 24 05 13	0.08 .63 .71 .27 13 .10 14 .12 13 19 15	-0.35 .44 .02 41 19 -2.18 09 24 36					

^aWashington, D. C.; specimens facing south on racks inclined at 45°. NACA

^bMethod No. 6023, Federal Specification L-P-406a (reference 2).

^cSpecimens cut lengthwise.

^dSpecimens cut crosswise.

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TABLE III. - STABILLTY RATINGS OF THE PLASTIC MATERIALS IN OUTDOOR WEATHERING,

ACCELERATED WEATHERING, AND ACCELERATED SERVICE TESTS

$\overline{}$	Τ		Ves	thering			T						<u>.</u>			·
Material	Accelerated			Accelerated			Accelerated service test-									
designe- tion	Out	door		6021 (o)		6023 (a)		I		1		m		IV		•
ļ	l yr	2 Jr	120 hr	240 hr	5 cg	10 cg	5 cg	10 cy	5 og	10 cg	5 cg	10 cy	5 cg	10 cy	5 cg	10 cy
Weight ^b																
	8 9 11 10 1 2 5.5 3 7 4 5.5	8 10 11 9 3 4 2 1 5 7 6	11 2 3 9 1 6 7 10 8 5	11 3 + 5 4 - 5 10 1 6 7 9 8 2	11 2 3 7 1 8 6 10 9 5	11 2 3 7 1 8 6 10 9 5	11 3 4 5 2 8 7 10 96	11 3 4 6 2 7-5 10 9 5	11 5689134072	116 78 91 34 10 52	111347268095	11.5 3 7.5 9 10.8 5	13218407965	12 1 38 4 10 7 9 6 5	11 24 5 7 16 9 10 8 3	13 4 57 16 9 18 2
							Leng	sth and w	14th ^b				_			. 122
Al Big Ci Di Fi HI IJ IJ	2.5 7.5 10 7.5 1 9 1 5 2.5	8.5 6.5 10 6.5 1 18.5 3 2	9.5 3.5 2 3.5 8 1 7 9.5 116 5	10 3.5 2 3.5 8.5 7 8.5 11 6	11 5 4 3 7 1 9 18 6 2	11 56 2 7.5 1 9 10 4 7.5 3	11 26.5 38 1.5 10 96.5 4.5	11 2 5 3 8 1 5 10 9 7 5	11 5 4 2.5 9 16 8 10 7 2.5	11 5 3 9.5 1 6 8 9.5 7	11 2.5 4.5 7 18 10 96 5	11 3 2 7 1 8 9.5 9.5 5	9 4.5 3 2 11 10 8 7 6	8 3 2 11 10 9 7 6 5	11 2.5 4 2.5 7 1 8 10 96 5	11 3.5 3.5 7 18.5 10 8.5 5
			·			-L	1	hickness	<u> </u>	!	<u> </u>		1			<u> </u>
Me Me Me Me Me Me Me Me Me Me Me Me Me M	30 11 97 486 215	4 10 11 9 7 3 8 6 2 1 5	7 2 8.5 10 18.5 5 3 11	784 1011 1926 53	10 11 19 4.5 26 34.5 7	5 10 7.5 1 7.5 3 11 2 4	2.5 10 11 96 2.5 78 51	6.5 10 11 95 38 6.5 2 1	6 10 9 11 8 1 7 3 5 2	7 10 9 11 8 16 4 35 2	11 2 5 4 9 6 5 10 5 2 8	11 1.5 3 10 8 6.5 5 1.5 6.5 9	11 9 10 7 8 4.5 2 4.5 3	1189710361542	9.5 9.5 9.5 16 2 7	11 10 4 6 8 7 1 9 3 2 5
·							Flex	ural str	ngth			•	-			
AL BH ^c CU III III III III III III	2 11 10 9 7 38 4 56 1	3 10 11 96.5 256.5 8 4 1	11 9 4 26 5 3 7 8 10 1	19753642H981	8 10 9 5.5 5.5 11 1 7 3 2	11 10 9 5 3 7 8 4 6 2 1	11996 78 315.4 81	19 10 8 6 7 3 5 4 2 1	6 5 38 11 7 10 9 1 2	8 4 5 36 11 70 9 1 2	11 6 8.5 10 4 5.5 7 2	8 9 11 3 7 2 5 10 6 4	11. 70. 69. 88. 54. 31.	17659389421	16 3 2 9 5 4 10 8 7 1	10 5 2 7 38 11 9 1
						Modul	വടവ് ല	asticity			<u> </u>					. –
AL BL [‡] CL DL EL DL EL DL DL EL DL DL EL DL DL EL DL DL EL DL DL DL DL DL DL DL DL DL DL DL DL DL	8 10 11 7 3 2 4 5 6 9 1	11 10 8 9 4.5 3 1 7 4.5 6 2	11 9 7 3 4 5 2 8 6 10 1	1184562197193	17 9 5 3 6 2 8 3 9 1	11 8 96 34 2 7 .5 10 1	11 8 9 3 4 2 6 5 7 10 1	1189732564 101	1076,35149812	17436929815	13965147892	16074238591	11 938 27 56 10 1	11 5 7 3 9 2 8 4 6 10 1	1168 4 5 1 3 9 7 10 2	11 6 7 3 5 2 8 9 1 10 1
Maximum deflection in flexure ^b																
Ale Mf CI DL EL EL LL JL	á	11 6 7.5 7.5 9 2 1 3 1	15987921346	H 4 96 10 8 2 1 3 5 7	10.5 6 8 9 5 10.5 4 2 1 7 3	11 10 96 8 1 4 37 2	117084392561	11 6 10 7 4 9 8 1 3 7 2	10 8 5.5 7 9 1 1 2 3 4 5.5	1996 78 11 14 235	11 7 9 8 4 10 3 1 26 5	11 219 97 4 5 1 6 8 3	17 17 17 17 17 17 17 17 17 17 17 17 17 1	11 7 9 8 5 10 3 1 1 6 2	11 9 10 8 7 3 2 1 4 6 5	11 8 10 9 6 7 1 1 3 2 5

Spata for tests other than the 2-year outdoor weathering and accelerated weathering by Method No. 6023 were taken from reference 1.

For changes in weight and dimensions the materials are rated according to the degree of change, the least change being denoted by a rating of 1. For the flemmal strength and the flemmal modulus of elasticity the materials are rated according to the retention of strength, the material with the greatest increase being rated 1 and that with the greatest decrease being rated 11.

For the maximum deflection in flemma the material with the greatest negative change is rated as 1 and that with the greatest positive change as 11.

Specimens cut lengthwise.

Specimens cut crosswise.

Method No. 6021, Federal specification L-F-406a (reference 2).

Method No. 6023, Federal Specification L-F-406a (reference 2).

TABLE IV. - CHANGES IN FLEXURAL STRENGTH, MODULUS OF ELASTICITY, AND MAXIMUM DEFLECTION IN FLEXURE OF PLASTICS DURING

OUTDOOR AND ACCELERATED WEATHERING TESTS

Material desig- nation	Initial strength (lb/sq in.), modulus (lb/sq in.), or deflection (mils)	Change during outdoor weathering test, 2 years (percent)	Changes during accelerated. weathering test (b) 5 10 cycles cycles									
		(a)	(percent)	(percent)								
Flexural strength												
AL BLC BL CL DL BL FL HL LL JL KL	12,700 42,600 29,000 25,100 23,500 34,100 16,100 13,100 22,900 17,400 9,000	-13.4 -37.6 -39.3 -35.3 -24.3 -2.6 -20.5 -24.4 -24.9 -18.4 8.6	-8.7 -14.3 -13.1 -4.6 -4.7 -17.9 -3.0 -6.6 1.1	-25.9 -18.5 -15.9 -7.7 -4.3 -11.1 -15.5 -6.9 -8.3 -1.2 3.3								
Modulus of elasticity in flexure												
Al. Bl° Bld Cl Dl Kl Fl Hl Il Jl Kl	1,170,000 3,363,000 1,845,000 2,567,000 1,920,000 1,810,000 706,000 652,000 1,238,000 1,121,000 986,000	-40.2 -34.8 -27.8 -29.4 -18.1 -7.1 2.0 -25.3 -18.2 -22.1 -1.9	-41.7 -16.3 -20.0 -13.5 -10.6 -14.4 -4.2 -17.5 -10.5 -22.0	-47.2 -18.9 -23.9 -16.0 -10.9 -13.6 -8.8 -17.9 -14.7 -25.3 13.8								
	. Maximum deflection in flexure											
AL BL CL DL EL FL HL IJ	24.0 26.4 31.0 27.4 21.5 45.7 72.7 68.2 65.2 41.2 21.0	41.7 -2.6 .0 .0 -10.2 5.0 -39.9 -40.2 -18.4 -13.8 6.2	43.3 11.4 21.9 24.8 8.5 7.2 -8.9 14.8 14.8	45.8 8.8 38.7 23.4 10.7 18.8 -8.2 3.7 -1.5 16.5 -4.8								

^aWashington, D. C.; specimens facing south on racks inclined at 45°. ^bMethod No. 6023, Federal Specification L-P-406a (reference 2). ^cSpecimens cut lengthwise. dSpecimens cut crosswise.